

Seminar on Adaptive Real-Time Systems, with emphasis on Real-Time Control Systems ontrol Dept. (ESAII), Technical University of Catalonia (UPC), Barcelona, June 20

## Real-time control systems





## Real-time control systems



 ... but we analyse control problems and offer solutions when required



Control

- We do not focus only on real-time issues... too difficult <sup>©</sup>
  - ... but we analyse real-time problems and offer solutions when required

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Real-time control systems







(20-25 participants)



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## Real-time control systems

#### 1. Control systems: the basics

... focuss on timing sensitive features

#### 2. Real-time computing of control systems

... do resource constraints affect control systems performance?

#### 3. Control of computing systems

... can control theory improve computing systems performance?

#### 4. Stability issues

... at least, everything has to be stable

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- 1. Concepts
- 2. Introductory examples
- 3. System poles
- 4. State Space Models
- 5. Discrete time systems, models and poles
- 6. Simulation
- 7. Controller design



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## Control systems: the basics Concepts

The **goal of control** is to apply inputs to a system in order to have the system behaving as expected/desired.

- Cruise-control car: f\_engine(t)=?  $\rightarrow$  speed=60 mph
- Utilization control in a video server : Admitted\_requests(h)?  $\rightarrow$  utilization=80%

#### Configurations

Input — plant _ Output	System to be contro	lled	
Desired output — Controller Input	plant→ Output	Open loc	p control
Desired output → Comparison → Co	ntroller Input plant	→ Output	Closed loop control

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### Concepts

**Open loop control** Desired output — Controller Input plant — Output

Idea: Compute control input without continuous\* variable measurement

- Simple
- Need to know EVERYTHING ACCURATELY to work right

Cruise-control car: friction(t), ramp\_angle(t)

video server: workload(h) (request arrival rate? decoding times?);

#### Open-loop control fails when

- We don't know everything
- · We make errors in estimation/modeling
- Things change



Closed loop control Desired output 
Comparison Controller Input plant Output

Idea: Compute control input as a function of continuous\* variable measurement

- More complicated (so we need control theory)
- Continuously measure & correct
  - Cruise-control car: measure speed & change engine force
  - Video server: measure utilization and completion rate & change admission rate

#### Feedback control theory makes it possible to control well even if

- · We don't know everything
- We make errors in estimation/modeling
- Things change

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# Control systems: the basics

#### Control design methodology





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# Control systems: the basics

### **Introductory examples**

Let's look at cruise control





• The **set/accel** button tells the car to maintain the speed you are currently driving at. Holding down the set/accel button will make the car accelerate

• Holding down the **coast** button will cause the car to decelerate

**Objective:** to accelerate to the desired speed without overshooting, and then to maintain that speed with little deviation no matter how much weight is in the car, or how steep the hill you drive up.



### **Introductory examples**





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## Control systems: the basics Introductory examples

### Let's look at cruise control: stable dynamics

First order differential equation  $u - bv = m\dot{v}$  y = v?

Going at 10km/h, if no force (u=0) is applied...



... the car slows down  $\Rightarrow$  the car is **stable** 

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### **Introductory examples**

#### Let's look at cruise control: stable dynamics

First order differential equation  $u - bv = m\dot{v}$  y = v?

Going at 10km/h, if no force (u=0) is applied...

Solution:  $v(t) = C \cdot e^{\frac{-b}{m} \cdot t}$ 

Proof:  $0 - b \cdot C \cdot e^{\frac{-b}{m} \cdot t} = m \cdot C \cdot \frac{-b}{m} \cdot e^{\frac{-b}{m} \cdot t}$ 

(if 
$$v(0)=10 \Rightarrow C=v_0=10$$
)

The shape of the response depends on the exponential coeficient



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## Introductory examples

#### Let's look at cruise control: dynamics

$$v(t) = v_0 \cdot e^{\frac{-b}{m}t}$$

If the friction increases (b $\uparrow$ ), the response will be faster If the mass increases (m $\uparrow$ ), the response will be slower



Note that the exponential coefficient is < 0



### **Introductory examples**

Summary: the exponent's coefficient determines the response shape.

The smaller is the coefficient the faster is the response  $v(t) = v_0 \cdot e^{m}$ 





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## Control systems: the basics

## **Introductory examples**

Let's look at rocket control



**Objective:** to keep a desired angle



### Introductory examples

#### Let's look at rocket control: model





# Control systems: the basics

## Introductory examples

#### Let's look at cruise control: unstable dynamics

Second order differential equation  $J\ddot{\theta} - b\dot{\theta} - m\theta = M_c$   $y = \theta$ ?

Initial angle of 0.0005 rad, if no force (M<sub>c</sub>=0) is applied...





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... the rocket starts rotating  $\Rightarrow$  the rocket is **unstable** 



### **Introductory examples**

#### Let's look at cruise control: unstable dynamics

First order differential equation  $J\ddot{\theta} - b\dot{\theta} - m\theta = M_c$   $y = \theta$ ?

With an initial angle of 0.0005 rad, if no force ( $M_c$ =0) is applied...

Solution:  $\theta(t) = C_1 \cdot e^{\frac{b + \sqrt{b^2 + 4Jm}}{2J}t} + C_2 \cdot e^{\frac{b - \sqrt{b^2 + 4Jm}}{2J}t} = C_1 \cdot e^{\lambda_1 t} + C_2 \cdot e^{\lambda_2 t}$ 

If initial conditons are:  $\theta(0)=0.0005$  \_\_\_\_\_  $d\theta/dt (0)=0$  \_\_\_\_\_ If part C1=0.0002323 J = 1 C2=0.0002676 b=1 m=5

If parameters are: J = 10kg⋅m2 b=1 Nsm m=5 Nm

 $\implies \begin{array}{c} \lambda_1 = 0.7589 \\ \lambda_2 = -0.6589 \end{array}$ 

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Once again, the shape of the response depends on the exponent's coefficients

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## Control systems: the basics

## Introductory examples

Let's look at rocket control: dynamics  $\theta(t) = C_1 \cdot e^{\lambda_1 t} + C_2 \cdot e^{\lambda_2 t}$ 

If coefficients  $\lambda$  are positive, the system is unstable (one would be enough) If coefficients  $\lambda$  are negative, the system is stable





Control systems: the basics System poles

General Case: differential equation or order n

$$a_n y^{n} + a_{n-1} y^{n-1} + \ldots + a_0 y = u$$

Solution:

$$y(t) = C_1 \cdot e^{\lambda_1 t} + C_2 \cdot e^{\lambda_2 t} + \ldots + C_n \cdot e^{\lambda_n t}$$

The shape of the response depends on the exponent's coefficients  $\lambda$ 

Stability: If any of these coefficients is positive the system will be unstable

These coefficients are called "System Poles"

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### State-space models

Example: Cruise control

 $u - bv = m\dot{v}$ 

 $\dot{v}(t) = \left[\frac{-b}{m}\right] v(t) + \left[\frac{1}{m}\right] u(t)$ y(t) = [1] v(t)

Example: rocket control

 $J\ddot{\theta} - b\dot{\theta} - m\theta = M_c$ 



General state space model (SISO)

 $\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}u(t)$  $y(t) = \mathbf{C}\mathbf{x}(t) + \mathbf{D}u(t)$ 

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$$\begin{array}{c} \theta = x_1 \\ \dot{\theta} = x_2 \end{array} \xrightarrow{x_1 = x_2} \\ \dot{x}_2 = \frac{b}{J}\dot{\theta} + \frac{m}{J}\theta + M_c = \frac{b}{J}x_2 + \frac{m}{J}x_1 + M_c \end{array}$$

$$\begin{bmatrix} \dot{\theta}_1(t) \\ \dot{\theta}_2(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ \frac{m}{J} & \frac{b}{J} \end{bmatrix} \begin{bmatrix} \theta_1(t) \\ \theta_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} M_C(t)$$
$$y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} \theta_1(t) \\ \theta_2(t) \end{bmatrix}$$



### **State-space models**

$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}u(t)$$
  
 $y(t) = \mathbf{C}\mathbf{x}(t) + \mathbf{D}u(t)$  Where are the system poles?

$$|\lambda I - A| = 0$$

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Characteristic equation

#### Example: rocket control

 $\begin{bmatrix} \dot{\theta}_1(t) \\ \dot{\theta}_2(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ \frac{m}{J} & \frac{b}{J} \\ \frac{m}{J} & \frac{b}{J} \end{bmatrix} \begin{bmatrix} \theta_1(t) \\ \theta_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} M_C(t)$ 

Model

 $y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} \theta_1(t) \\ \theta_2(t) \end{bmatrix}$ 

$$|\lambda I + A| = \begin{vmatrix} \lambda & 0 \\ 0 & \lambda \end{vmatrix} - \begin{bmatrix} 0 & 1 \\ \frac{m}{J} & \frac{b}{J} \end{vmatrix} = 0$$
$$\left[ \begin{pmatrix} \lambda & -1 \\ -\frac{m}{J} & \lambda - \frac{b}{J} \\ \frac{1}{J} \end{pmatrix} \right] = 0$$
$$\lambda(\lambda - \frac{b}{J}) - \frac{m}{J} = 0$$
$$\lambda^{2} - \frac{b}{J}\lambda - \frac{m}{J} = 0$$

Solution:  
$$\lambda = \frac{b \pm \sqrt{b^2 + 4Jm}}{2J}$$

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## Control systems: the basics Summary

System poles determine stability shape of the response

State space models ... continuous

Computers have a discrete view of the world !!!!



## Discrete time systems, models and poles





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## Control systems: the basics

## Discrete time systems, models and poles

The computer has a discrete view of the plant  $\Rightarrow$  the control algorithm has to be designed taking into account that it will "deal with" sequences of numbers  $\Rightarrow$  a discrete model of the plant is required.

The most commonly used model assumes:

- equidistant sampling: h sampling period (seconds)
- instantaneous input-to-output latency



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## Discrete time systems, models and poles

Continuous time model

Discrete time model

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 $\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}u(t) \qquad \mathbf{x}_{kh+h} = \mathbf{\Phi}\mathbf{x}_{kh} + \mathbf{\Gamma}u_{kh}$  $y(t) = \mathbf{C}\mathbf{x}(t) + \mathbf{D}u(t) \qquad \uparrow \qquad \mathbf{x}_{kh+h} = \mathbf{C}\mathbf{x}_{kh} + \mathbf{D}u_{kh}$  $\Phi = e^{Ah}$  $\Gamma = \int_{a}^{b} e^{\mathbf{A}s} ds \mathbf{B}$ 

Computing  $\Phi$  and  $\Gamma$ :

- Symbolically
- Series expansion of the exponential matrix
- Numerically (Matlab)



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### **Discrete time systems, models and poles**





### Discrete time systems, models and poles



Rocket model: we have to operate until we obtain the desired accuracy

- For the rocket model (simple model), with i=5, we obtain 2 correct decimals

- depending on the model (e.g., stable plants), the expansion works very well

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### **Discrete time systems, models and poles**

Note that the most commonly used model assumptions:

- equidistant sampling: h sampling period
  - instantaneous input-to-output latency

are not real

Computations (or network) take time (input-to-output latency=0)



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## Control systems: the basics

## Discrete time systems, models and poles

#### NCS (networked control systems)



Communication network



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## Control systems: the basics

### Discrete time systems, models and poles





## Control systems: the basics State-space models

$$\mathbf{x}_{kh+h} = \mathbf{\Phi} \mathbf{x}_{kh} + \mathbf{\Gamma} u_{kh}$$
$$y_{kh} = \mathbf{C} \mathbf{x}_{kh} + \mathbf{D} u_{kh}$$

Where are the system poles?

$$\lambda \mathbf{I} - \mathbf{\Phi} = 0$$

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Characteristic equation

#### Example: rocket control

#### Simple model

æ	1.7839	2.0143
Φ=	2.0143	3.7982

$$\begin{vmatrix} \lambda I + \Phi \end{vmatrix} = \begin{bmatrix} \lambda & 0 \\ 0 & \lambda \end{bmatrix} - \begin{bmatrix} 1.7839 & 2.0143 \\ 2.0143 & 3.7982 \end{bmatrix} = 0 \\ \begin{vmatrix} \lambda - 1.7839 & -2.0143 \\ -2.0143 & \lambda - 3.7982 \end{vmatrix} = 0 \\ (\lambda - 1.7839)(\lambda - 3.7982) - (-2.0143)^2 = 0 \\ \lambda_1 = 0.5390 \\ \lambda_2 = 5.0432 \end{vmatrix}$$

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## Control systems: the basics

### Discrete time systems, models and poles

#### Correspondence between continuous time poles vs. discrete time poles: Cruise control example





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## Control systems: the basics

### **Simulation**



t=0:15 plot(t,0.0002323\*exp(0.7589\*t)+0.0002676\*exp(-0.6589\*t))





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Control systems: the basics

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	0 6 8 8 8 1 8 8 2	○ ► ■ Normal ▼	Block Parameters: D	15	·····-
$discrete \\ \begin{bmatrix} \theta_1(k+1) \\ \theta_2(k+1) \end{bmatrix} = v(k) = \begin{bmatrix} 1 & 0 \end{bmatrix}$	Image: second system       Image: second system <t< th=""><th><math display="block">(x_{(n)}+Du_{(n)}) = Normal</math> <math display="block">(x_{(n)}+Du_{(n)}) = Ax_{(n)}+Bu_{(n)}</math> <math display="block">(x_{(n)}+Bu_{(n)}) = Scope</math> <math display="block">(100\%)</math> <math display="block">(x_{(k)}) = \left( \begin{array}{c} 0.5391 \\ 1.1416 \end{array} \right) M_{C}(k)</math></th><th>Block Parameters: D           Discrete State Space           x(n+1) = Ax(n) + Bu(ny(n)) = Cx(n) + Du(ny(ny(ny(ny(ny(ny(ny(ny(ny(ny(ny(ny(ny(</th><th>15 10 5 0 0 5 Time offset: 0 5 5 5 5 5 5 5 5 5 5 5 5 5</th><th></th></t<>	$(x_{(n)}+Du_{(n)}) = Normal$ $(x_{(n)}+Du_{(n)}) = Ax_{(n)}+Bu_{(n)}$ $(x_{(n)}+Bu_{(n)}) = Scope$ $(100\%)$ $(x_{(k)}) = \left( \begin{array}{c} 0.5391 \\ 1.1416 \end{array} \right) M_{C}(k)$	Block Parameters: D           Discrete State Space           x(n+1) = Ax(n) + Bu(ny(n)) = Cx(n) + Du(ny(ny(ny(ny(ny(ny(ny(ny(ny(ny(ny(ny(ny(	15 10 5 0 0 5 Time offset: 0 5 5 5 5 5 5 5 5 5 5 5 5 5	
$y(k) = \begin{bmatrix} 1 & 0 \end{bmatrix}$	$\theta_{2}(k)$		1		
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Matlab	8	Simulation			
con	tinuous	25	Response to Initial Co	onditions	
$\begin{bmatrix} \dot{\theta}_1(t) \\ \dot{\theta}_2(t) \end{bmatrix} = \begin{bmatrix} 0 \\ 0.5 \end{bmatrix}$ $y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}$	$\begin{bmatrix} 1\\ 0.1 \end{bmatrix} \begin{bmatrix} \theta_1(t)\\ \theta_2(t) \end{bmatrix} + \begin{bmatrix} 0\\ 1 \end{bmatrix} M_C(t)$ $\begin{bmatrix} t\\ t \end{bmatrix}$	20 -			
A=[0 1;0.5 B=[0;1]; C=[1 0]; D=[0]; sys=ss(A, initial(sys,	5 0.1]; B,C,D); [0.0005;0],15)	10 - 5 -			

0

0

5

Time (sec)

10

15



### Simulation

#### Matlab

#### discrete





# Control systems: the basics

## **Control design**

The objective of control is to shape the system response

Pole placement by state feedback allows to specify arbitrary pole locations

Example (Open loop) plant (simple model)

 $\begin{bmatrix} \theta_1(k+1) \\ \theta_2(k+1) \end{bmatrix} = \begin{bmatrix} 1.7893 & 2.0143 \\ 2.0143 & 3.7982 \end{bmatrix} \begin{bmatrix} \theta_1(k) \\ \theta_2(k) \end{bmatrix} + \begin{bmatrix} 0.7839 \\ 2.0143 \end{bmatrix} M_C(k)$ 

A linear feeback can be described by

$$M_{C}(k) = -l_{1}\theta_{1}(k) - l_{1}\theta_{1}(k) = -\begin{bmatrix} l_{1} & l_{2} \end{bmatrix} \begin{bmatrix} \theta_{1}(k) \\ \theta_{2}(k) \end{bmatrix}$$

With this feedback, the closed loop system becomes

$$\begin{bmatrix} \theta_1(k+1) \\ \theta_2(k+1) \end{bmatrix} = \begin{bmatrix} 1.7893 & 2.0143 \\ 2.0143 & 3.7982 \end{bmatrix} \begin{bmatrix} \theta_1(k) \\ \theta_2(k) \end{bmatrix} + \begin{bmatrix} 0.7839 \\ 2.0143 \end{bmatrix} \left( -\begin{bmatrix} l_1 & l_2 \end{bmatrix} \begin{bmatrix} \theta_1(k) \\ \theta_2(k) \end{bmatrix} \right)$$

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## **Controller design**

(example continuation)

 $\begin{bmatrix} \theta_1(k+1) \\ \theta_2(k+1) \end{bmatrix} = \begin{bmatrix} 1.7893 - 0.7839l_1 & 2.0143 - 0.7839l_2 \\ 2.0143 - 2.0143l_1 & 3.7982 - 2.0143l_2 \end{bmatrix} \begin{bmatrix} \theta_1(k) \\ \theta_2(k) \end{bmatrix}$ 

Characteristic equation  $|\lambda \mathbf{I} - \mathbf{\Phi}| = 0$ 

 $\begin{vmatrix} \lambda \mathbf{I} - \begin{bmatrix} 1.7893 - 0.7839l_1 & 2.0143 - 0.7839l_2 \\ 2.0143 - 2.0143l_1 & 3.7982 - 2.0143l_2 \end{bmatrix} = 0$ 

 $\lambda^{2} + (0.7839l_{1} - 5.5821 + 2.0143l_{2})\lambda + 2.7182 + 1.0799l_{1} - 2.0143l_{2} = 0$ 

We know that stability requires to have system poles  $|p_i| < 0$ . Let's arbitrarely choose

 $p_1 = 0.4 + 0.4i$  and  $p_2 = 0.4 - 0.4i$ 

The desired characteristic equation is  $(\lambda - (0.4 + 0.4i))(\lambda - (0.4 - 0.4i)) = \lambda^2 - 0.8\lambda + 0.32 = 0$ 

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## Control systems: the basics

## **Controller design**

(example continuation)

Characteristic equation

 $\lambda^2 + (0.7839l_1 - 5.5821 + 2.0143l_2)\lambda + 2.7182 + 1.0799l_1 - 2.0143l_2 = 0$ 

The desired characteristic equation is

$$\lambda^2 - 0.8\lambda + 0.32 = 0$$

Equating equations coefficients 
$$\frac{0.783}{2.715}$$

$$0.7839l_1 - 5.5821 + 2.0143l_2 = -0.8 \qquad l_1 = 1.2790$$
  
$$0.7182 + 1.0799l_1 - 2.0143l_2 = 0.32 \qquad l_2 = 1.8763$$

Closed loop system equation

$$\begin{bmatrix} \theta_1(k+1) \\ \theta_2(k+1) \end{bmatrix} = \begin{bmatrix} \Phi - \Gamma L \end{bmatrix} \begin{bmatrix} \theta_1(k) \\ \theta_2(k) \end{bmatrix} = \begin{bmatrix} 0.7813 & 0.5434 \\ -0.5620 & 0.0187 \end{bmatrix} \begin{bmatrix} \theta_1(k) \\ \theta_2(k) \end{bmatrix}$$



## **Controller design**

#### Matlab (simple model)



Ld=[0.9743 1.1633]

[Phi,Gamma,dC,dD]=ssdata(dsys); poles=[0.4 + 0.4i,0.4 - 0.4i]; Ld=acker(Phi,Gamma,poles) cldsys=ss(Phi-Gamma\*Ld,Gamma,dC,dD,1);

initial(cldsys,[0.0005;0]) //WRONG//

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Time (sec)

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### **Controller design**

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x<sub>0</sub>=[0;0]

☑ Interpret vector parameters as 1-D

Cancel

Help

0K





## **Controller design**

#### Summary

- Controller design  $L=acker(\Phi,\Gamma,[p_1, p_2, ..., p_n])$
- p<sub>i</sub> are the desired pole locations of the closed-loop system
- Questions: Where do we place the desired poles?

What about the sampling period or execution time (i.e., control tasks timing constraints)?



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## Real-time computing of control systems

- 1. Controller implementation
- 2. Selection of the control task period
- 3. Trading off performance vs. schedulability
- 4. The jitter problem
- 5. Flexible timing constraints



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## Real-time computing of control systems

## **Controller implementation**

The controller is an algorithm to be executed at each sampling period h



Which is the right code?



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## Real-time computing of control systems

## **Controller implementation**

The controller is an algorithm to be executed at each sampling period *h* 

#### Attempt 1:

LOOP

PeriodicActivity; WaitTime(h);

END;

- Does not work.
- Both, Period *h* and PeriodicActivity, time-varying.
- The execution time of PeriodicActivity is not accounted for.



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Real-time computing of control systems

## **Controller implementation**

The controller is an algorithm to be executed at each sampling period h

#### Attempt 2:

LOOP

Start = CurrentTime(); PeriodicActivity; Stop = CurrentTime(); C := Stop - Start; WaitTime(h - C);

END;

• Does not work. An interrupt causing suspension may occur between the assignment and WaitTime.

• In general, a WaitTime (Delay) primitive is not enough to implement periodic processes correctly.

• A WaitUntil (DelayUntil) primitive is needed.



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## Real-time computing of control systems

## **Controller implementation**

The controller is an algorithm to be executed at each sampling period h

#### Attempt 3:

t = CurrentTime(); LOOP PeriodicActivity; t = t + h; WaitUntil(t); END;

• Will try to catch up if the actual execution time of PeriodicActivity occasionally becomes larger than the period (a too long period is followed by a shorter one to make the average correct)

• Reasonable for alarm clocks, but perhaps not for controllers.

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Real-time computing of control systems

### **Controller implementation**

#### Computer-control theory timing assumptions:





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Real-time computing of control systems

## **Controller implementation**

Keeping control timing assumptions with real-time task timing constraints

#### Standard timing constraints for periodic tasks





## Real-time computing of control systems

## **Controller implementation**

#### Limits control task scheduling



#### Scheduling *n* control tasks

*n* = 1 ok

n > 1 in the general case, not possible

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### Problem

Computer-control theory timing assumptions

Over-constrain control task specification

Poor (or infeasible) system schedulability



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Real-time computing of control systems

### **Controller implementation**

#### **Computer-control theory timing assumptions:**



#### Control task model (new)

Sampling and actuation are performed by hardware interrupts, control algorithm computation is implemented in a periodic tasks.

## At the end, it will present the same problems as the previous models

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## Real-time computing of control systems

## **Controller implementation**





## Real-time computing of control systems

### **Controller implementation**

Truetime Example1: a periodic task with period 10ms, execution time 2ms, under RM

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## Real-time computing of control systems

## **Controller implementation**

Truetime: *Example1*:

a periodic task with period 10ms, execution time 2ms, under RM, that increments a counter



example1\_init.m

taskcode.m



Real-time computing of control systems

### **Controller implementation**

**Truetime:** *Example1*: a periodic task with period 10ms, execution time 2ms, under RM, that increments a counter





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## Real-time computing of control systems

### **Controller implementation**

Truetime: Example2:

two periodic tasks with periods 10 and 14ms, execution times 2 and 4ms, under RM, each one increments a counter

<mark>₩ Example2 *</mark> File Edit View Simul C   C 및 A (C)	ation Format Tools Help 炎 暗 電   ニ ニ   ト = Normal		
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Real-time computing of control systems

### **Controller implementation**

Truetime: Example2:

two periodic tasks with periods 10 and 14ms, execution times 2 and 4ms, under RM, each one increments a counter

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### **Controller implementation**

Truetime: Example2:

two periodic tasks with periods 10 and 14ms, execution times 2 and 4ms, under RM, each one increments a counter





## Real-time computing of control systems

### **Controller implementation**



Truetime: *Example3*: the rocket controller task



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## Real-time computing of control systems

## **Controller implementation**

Truetime: Example3:

the rocket controller task

lock Parameters: State-Space 🛛 🛛 🔀	Block Parameters: Pulse Generator
State Space	Pulse Generator
State-space model: dx/dt = Ax + Bu y = Cx + Du	Generate pulses at regular intervals where the pulse type determines the computational technique used.
Parameters A:	Sample-based is recommended for use with a fixed step solver or within a discrete portion of a model using a variable step solver.
[0 1;0.5 0.1]	Parameters
B:	Pulse type: Time based
[0;1]	Amplitude:
C.	0.23
[1 0;0 1]	Period (secs):
D:	20
[0; 0]	Pulse Width (% of period):
Initial conditions:	0.01
[0.0005;0]	Phase delay (secs):
Absolute tolerance:	0.5
auto	✓ Interpret vector parameters as 1-D
OK Cancel Help Apply	OK Cancel Help Apply


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Real-time computing of control systems

#### **Controller implementation**

Truetime: *Example3*: the rocket controller task



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## Real-time computing of control systems

### **Controller implementation**

Truetime: Example3: the

the rocket controller task



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2										_
1.5										
1										
0.5	i 1	2	3	4	5	i 6	7	8	9	10
Time offset:	0									

• What happens when the delay increases? Why (check poles)?



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Real-time computing of control systems

### **Controller implementation**

**Truetime:** *Example3*: the rocket controller task (with delay of 0.4s)





## Real-time computing of control systems

### **Controller implementation**

Analysis: *Example3*: the rocket controller task (with delay of 0.4s)

Poles of the closed loop system without delays



A=[0 1;0.5 0.1];B=[0;1];C=[1 0];D=[0]; sys=ss(A,B,C,D) dsys=c2d(sys,1,'zoh'); [Phi,Gamma,dC,dD]=ssdata(dsys) poles=[0.4 + 0.4i,0.4 - 0.4i] Ld=acker(Phi,Gamma,poles) cldsys=ss(Phi-Gamma\*Ld,Gamma,dC,dD,1); p=pole(cldsys); t=0:1/10:6.5; y=sin(t); x = cos(t);plot(x,y)hold on plot(real(p(1)),imag(p(1)),'Marker','x') plot(real(p(2)),imag(p(2)),'Marker','x') hold off

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### **Controller implementation**

Analysis : *Example3*: the rocket controller task (with delay of 0.4s)

Poles of the closed loop system without delays: system with delay





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## Real-time computing of control systems

## **Controller implementation**

**Analysis :** *Example3*: the rocket controller task (with delay of 0.4s)





### **Controller implementation**

Analysis : *Example3*: the rocket controller task (with delay up to 0.3s)

Poles of the closed loop system without delays: system with delay  $(z_{kh}=u_{kh-h})$ 





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## Real-time computing of control systems

## **Controller implementation**

Analysis : Example3: th

the rocket controller task (with delay of 0.4s)





#### **Controller implementation**





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## Real-time computing of control systems

### **Controller implementation**

Analysis : *Example3*:

the rocket controller task (with delay of 0.4s)





### **Controller implementation**







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## Real-time computing of control systems

## **Controller implementation**

**Truetime :** *Example3*: the rocket controller task (with delay of 0.4s)

Block Parameters: State-Space	Block Parameters: Pulse Generator
State Space State-space model: Model parameters as be dx/dt = Ax + Bu y = Cx + Du	fore Pulse Generator Generate pulses at regular intervals where the pulse type determines the computational technique used.
Parameters A:	I ime-based is recommended for use with a variable step solver, while Sample-based is recommended for use with a fixed step solver or within a discrete portion of a model using a variable step solver.
[01;0.5 0.1] B·	Parameters
5. [[0];1]	Amplitude:
C:	0.23
D:	
[0; 0]	Pulse Width (% of period):
Initial conditions:	J0.01
[[0.0005;0]	Phase delay (secs):
Absolute tolerance:	0.5
auto	✓ Interpret vector parameters as 1-D
OK Cancel Help Apply	OK Cancel Help Apply



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Real-time computing of control systems

#### **Controller implementation**

**Truetime :** *Example3*: the rocket controller task (with delay of 0.4s)



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#### **Controller implementation**

**Truetime :** *Example3*: the rocket controller task (with delay of 0.4s)





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## Real-time computing of control systems

## **Controller implementation**

**Truetime :** *Example3*: the rocket controller task (with delay of 0.4s) with simulink







### **Controller implementation**

#### Summary

- care must be taken with the effects of the controller execution time (delay)
- task deadline should be equal to task worst case execution time (to bound delays)

Let's look at the sampling period (= task period)



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## Real-time computing of control systems

### Selection of the control task period

## Closed loop system poles and sampling period (i.e., control task period) determine performance

Correct affirmations:

- Poles determine system response
- Poles determine the choice of the sampling period
- · Sampling period determines poles
- · Sampling period determines system response

From where do we start? Poles



### Selection of the control task period

Where do we place closed-loop system poles?

Classical design rules:

- Reduce the expected behavior of high order systems to 2nd order systems by placing two "slow" poles (in continuous time domain). Place the remaining (continuous time) poles in such way that the output behaves as expected (like the two slow poles would determine)
- 2.- Choose a sampling period according to the continuous time pole position
- 3.- Compute the discrete feedback law

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## Real-time computing of control systems

### Selection of the control task period

## Reduce the expected behavior of high order systems to 2nd order systems by placing two "slow" poles (in continuous time domain). Why?





• Fast poles (the smallest) don't affect too much. Any high order system behavior is seen as a second order system behavior

 Slow poles (also called dominant) determine the output

#### Selection of the control task period

Reduce the expected behavior of high order systems to 2nd order systems by placing two "slow" poles (in continuous time domain). Why?





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## Real-time computing of control systems

### Selection of the control task period

## Choose a sampling period (if possible) according to the continuous time pole position

• There are several rules-of-the-thumb for selecting the sampling period

- ...and extended practice tells that the sampling period should accomplish that the number of samples (N) should be at least 10 to 20  $\,$ 

$$N = \frac{2\pi}{\omega_n h \sqrt{1 - \zeta^2}}$$

where  $\omega_n$  is the natural (oscillation) frequency and  $\zeta$  is the damping coefficient of the desired closed-loop respose (given by the two slow poles)

The relation betwen these parameters,  $\omega_n$  and  $\zeta$ , and continuos time poles  $s_{1,2}$  is:

$$(\lambda - s_1)(\lambda - s_2) = 0$$
  
$$\lambda^2 + 2\zeta \omega_n \lambda + \omega_n^2 = 0$$



### Selection of the control task period

## Choose a sampling period (if possible) according to the continuous time pole position

Also fast poles determine sampling period

An extended rule-of-the-thumb for fast poles is that the sampling period should be 10 to 20 times smaller than the period at the natural frequency

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## Real-time computing of control systems

### Selection of the control task period

#### Compute the discrete feedback law

Use the technique shown before:

Convert the selected continuous poles to discrete ones



• Compute the gains (using ackerman's formula)



### Selection of the control task period

#### Servo positioning





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## Real-time computing of control systems

## Selection of the control task period

#### Period selection:

- **Pole positions** 
  - z1 = -100 + 300iz2 = -100 300i
  - z3 = -500

#### **Characteristic equation**

 $(\lambda + 100 + 300i)(\lambda + 100 - 300i) = 0$  $\lambda^{2} + 200\lambda + 100000 = 0$  $\lambda^{2} + 2\xi\omega_{n}\lambda + \omega_{n}^{2} = 0$  $\omega_{n} = 100\sqrt{10}$  $\xi = \frac{1}{\sqrt{10}}$ 



h = 0.0001s

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## Real-time computing of control systems

### Selection of the control task period

#### Matlab Code:





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## Real-time computing of control systems

### Trading off performance vs. schedulability

The sampling period usually has restrictions, e.g. in EDF,  $\sum ci/Ti < 1$ 

The processor in charge of the rocket angle control, may be also in charge of:

 Trajectory Nozzle aperture Engine temperature Power Gyroscopes •...

There are many tasks to be executed, and limited resources (processors, network...)

This problem becomes more critical for mass-marked products (i.e. mobile phones, automotive components, etc...) subject to hard economic constraints

Usually there is a minimum sampling period



### Trading off performance vs. schedulability



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#### Trading off performance vs. schedulability

#### Servo positioning when minimum sampling is fixed:





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## Real-time computing of control systems

### Trading off performance vs. schedulability

#### Degradation due to sampling period selection:

For a first order system, the solution is exact at the sampling points, but there is a degradation between them.



### Trading off performance vs. schedulability

#### Degradation due to sampling period selection:

For higher order systems, the degradation also implies exact solutions at the sampling points. The system behaves as expected only at the sampling points, and thus we obtain worst responses.

The lower the density of sampling points, the higher the difference between the desired and the real response



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## Real-time computing of control systems

### Trading off performance vs. schedulability

To evaluate the degradation we use indexes that reflect how much time the system needs to converge towards the setpoint and how far it is from the set point during this time. A commonly used index is the IAE (Integral of the Absolute value of the Error)

$$IAE = \int_0^\infty |y(t)| dt$$
$$IAE = \int_0^\infty |Y_d(t) - y(t)| dt$$



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### The jitter problem

General purpose scheduling policies  $\longrightarrow$  Inherent jitter in task instance execution

#### **Real-time interpretation:**

varying start time delays

varying response times



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# Real-time computing of control systems The jitter problem

#### **Control interpretation:**

- Sampling jitter: different values for the sampling period
- **Sampling-actuation jitter:** different values for the time delay





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## Real-time computing of control systems

### The jitter problem

#### Design stage

#### System run time

Computer-control timing assumptions

- **Constant** sampling period
- Constant time delay

Varying sampling periods

Scheduling inherent jitters

Varying time delays

Run time violation of the closed-loop timing assumptions

#### **Problem**

Standard scheduling schemes

Variability in task instance execution

Closed-loop performance degradation

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### The jitter problem

Example

#### System



Inverted pendulum

#### Controller

- Design: classical pole placement
- (to recover from a perturbation in less than 2s)
- Implementation: periodic task

#### Response (task executed in isolation)





## The jitter problem

#### Example





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## Real-time computing of control systems

### The jitter problem

#### Solution approach





### The jitter problem

#### Offline schedule analysis



#### **Jitter variability**

Sampling intervals	60	80	100	60	90	80	70	80	90	80	70	90	70	80	100
Sampling-actuation delays	20	20	20	20	20	30	30	20	40	20	20	20	20	30	20

h={60,70,80,90,100} (ms) τ={20,30,40} (ms)

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### The jitter problem

#### Offline control analysis

h={60,70,80,90,100} (ms) τ={20,30,40} (ms)

- Classically designed controller, -L(h, τ)
- Stability analysis -L(h,τ)

#### **Practical aspects**

Computational overhead (for the run time recalculation strategy)

	Traditional design	Compensation approach design
Number of Flops	60	2000

Memory requirements (for the run time table look-up strategy)

10Kb approx.

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## Real-time computing of control systems

### The jitter problem

#### Offline control analysis

*Regularly* sampled discrete-time systems with *constant* time delays

$$\begin{aligned} x(kh+h) &= \Phi(h)x(kh) + \Gamma_0(h,\tau)u(kh) + \\ &\Gamma_1(h,\tau)u(kh-h) \\ y(kh) &= Cx(kh) + Du(kh) \\ u(kh) &= -L(h,\tau)x(kh) \end{aligned}$$

#### **Closed-loop matrix:**

 $\Phi_{cl} = \begin{bmatrix} \Phi(h) - \Gamma_0(h,\tau) \cdot L(h,\tau) & \Gamma_1(h,\tau) \\ -L(h,\tau) & 0 \end{bmatrix}$ 

#### System evolution (kth iteration):

$$x(kh+h) = \Phi_{cl}x(kh) = \Phi_{cl}\Phi_{cl}^{k-1}x(kh-h) = \Phi_{cl}^{k}x(0)$$

*Irregularly* sampled discrete-time systems with *varying* time delays

$$x(t_{k+1}) = \Phi(h_j)x(t_k) + \Gamma_0(h_j, \tau_j)u(t_k) + \Gamma_1(h_j, \tau_j)u(t_{k-1})$$
$$y(t_k) = Cx(t_k) + Du(t_k)$$
$$u(t_k) = -L(h_j, \tau_j)x(t_k)$$

#### **Closed-loop matrix:**

$$\Phi_{clk} = \begin{bmatrix} \Phi(h_j) - \Gamma_0(h_j, \tau_j) \cdot L(h_j, \tau_j) & \Gamma_1(h_j, \tau_j) \\ -L(h_j, \tau_j) & 0 \end{bmatrix}$$

System evolution (kth iteration):

$$x(t_{k+1}) = \Phi_{cl_k} x(t_k) = \Phi_{cl_k} \Phi_{cl_{k-1}} \Phi_{cl_{k-2}} \dots \Phi_{cl_1} x(0)$$
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### The jitter problem

Offline control analysis

 $x(t_{k+1}) = \Phi_{cl_k} x(t_k) = \Phi_{cl_k} \Phi_{cl_{k-1}} \Phi_{cl_{k-2}} \dots \Phi_{cl_1} x(0)$ 

Stability analysis (depends on the implementation)

one closed-loop matrix

stable  $\Leftrightarrow \rho(\Phi_{cl}) \leq 1$ 

an infinite product of closed-loop matrices that follow a periodic pattern

stable  $\Leftrightarrow \rho(\Phi_{cl_1} \cdot \Phi_{cl_2} \cdot ... \cdot \Phi_{cl_n}) < 1$ 

**a** an infinite product of closed-loop matrices taken randomly from a finite set,  $\Omega$ 

Necessary and sufficient stability condition:  $\Omega$  stable  $\Leftrightarrow \exists P>0$ :  $\Phi^{\mathsf{T}}_{\mathsf{cl}_k} \cdot P \cdot \Phi_{\mathsf{cl}_k} - P<0$ ,  $\forall \Phi_{\mathsf{cl}_k} \in \Omega^k$ ,  $k \ge 1$ Sufficient stability condition (I): if  $\exists P>0$ :  $\forall \Phi_{\mathsf{cl}_k} \in \Omega$ ,  $\Phi^{\mathsf{T}}_{\mathsf{cl}_k} \cdot P \cdot \Phi_{\mathsf{cl}_k} - P<0 \Rightarrow$  stable Sufficient stability condition (II): if  $\forall \Phi_{\mathsf{cl}_k} \in \Omega : \Phi^{\mathsf{T}}_{\mathsf{cl}_k} \cdot \Phi_{\mathsf{cl}_k} - I<0 \Rightarrow$  stable



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## Real-time computing of control systems

### The jitter problem

Compensation approach basic idea

Controller parameters adjustment at each control task instance execution according to both actual sampling interval and sampling-acutation delay

-L(h<sub>k</sub>,τ<sub>k</sub>)

#### Key point: online parameters adjustment

Through online parameters recalculation (if negligible overhead)

Through online access to controller parameters look-up table (if not negligible overhead)



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## Real-time computing of control systems

### The jitter problem

#### Computational overhead analysis

Depends on [ the system to be controlled

the controller design method

#### **Examples**

Pole placement observer state feedback controller design for the inverted pendulum: O(n<sup>4</sup>)

	Number of Flops (without extra calculations)	Number of Flops (with extra calculations)
simplified pendulum (2x2 matrix)	25	250
complete pendulum (4x4 matrix)	60	2000

PID controller design for a DC servo: insignificant



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 $\tau_k \leq h_{max}$ 

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## Real-time computing of control systems

## The jitter problem

#### Memory requirements analysis

Size(table)=  $(h_{max} - h_{min})^*h_{max}^*$ clockticksize \* size(controller parameters)

Sampling interval variability:	$\boldsymbol{h}_{min} \! \leq \boldsymbol{h}_k \! \leq \! \boldsymbol{h}_{max}$
Sampling-actuation delays variability:	$0 \leq \tau_{\mu} \leq h_{max}$

Clockticksize (granularity)

#### Inverted pendulum example:

h <sub>k</sub> (ms)	τ <sub>k</sub> (ms)	-L(h <sub>k</sub> , τ <sub>k</sub> )
60	20	-L(60, 20)
70	20	-L(70, 20)
70	30	-L(70, 30)
90	20	-L(80, 20)
00	30	-L(80, 30)
00	20	-L(90, 20)
90	40	-L(90, 40)
100	20	-L(100, 20)



### The jitter problem

Key point: run-time controller parameters adjustment

Implementation issues: Slightly modification in the controller code

Generic controller							
{ read_inputs $(y(t_k), r(t_k));$	{						
$\mathbf{e}(t_k) = r(t_k) - y(t_k);$							
$u(t_k) = calculate_output (L(h, \tau), e(t_k));$							
write_output (u(t <sub>k</sub> ));							
}	}						

Compensation approach controller { read\_inputs  $(y(t_k), r(t_k));$ obtain  $(h_j, \tau_j);$   $e(t_k) = r(t_k) - y(t_k);$ obtain  $(L(h_j, \tau_j));$   $u(t_k) = calculate_output (L(h_j, \tau_j), e(t_k));$ write\_output  $(u(t_k));$ }

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### **Flexible timing constraints**

#### **Problem formulation**

- Standard scheduling schemes are based on fixed timing constraints (T, D)
- Fixed means that a single value for a constraint holds for all instances of a task

#### Flexibility

We do not want to set single values for the timing constraints, we want provide ranges of values to choose from

#### Compensation approach timing assumptions:

- Set of sampling intervals
- Set of sampling-actuation delays



Idea: to derive new timing constraints for control tasks

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## Real-time computing of control systems

## **Flexible timing constraints**

#### Flexible timing constraints for control tasks designed with compensations

Compensation approach		Flexible timing constraints
		Instance separations:
Set of sampling periods: h <sub>j</sub>	$\Rightarrow$	$\forall task_k, task_{k+1}: s(task_{k+1}) - s(task_k) \in set$
		Response times:
Set of delays: $\tau_j$		$\forall task_k$ : f(task_k) - s(task_k) \in set

Several values for a constraint are eligible at each task instance execution

#### **Example**

- two instances separations
- three response times

can be selected at each instance execution



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#### **Flexible timing constraints**

**Solved problem:** Poor system schedulability due to the application of fixed timing constraints for control tasks

#### Idea

characterize control tasks with flexible timing constraints, and

exploit their flexibility to improve system schedulability

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## Real-time computing of control systems

#### **Flexible timing constraints**





a computing of control evetom

## Real-time computing of control systems

### **Flexible timing constraints**



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# Real-time computing of control systems Summary

- relation between control task timing constraints and control system properties
- impact of scheduling methods on control performance: closed-loop systems degradation
- impact of classic control requirements on schedulabiliy: poor system schedulability
- compensation approach as a control-based solution
- flexible timing constraints to improve task set schedulability



- 1. Introduction
- 2. Key aspects in "control of RT control systems"
- 3. Slack reclaiming: optimal state feedback
- 4. Overload conditions

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## Control of computing systems Key aspects in "control of RT control systems"

- Controller design
- Type of control desing
- Possibility of controller adaptation
- Intuitive guidelines for co-design

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## Key aspects in "control of RT control systems"

To control (improve) a RT control system, we need a means of evaluation

#### IAE (Integral of the Absolute value of the Error)



### Key aspects in "control of RT control systems"

IAE can be evaluated for a set of sampling periods This can be either applied to:

- adapted controllers
- non adapted controllers

#### For adapted controllers

For(h=0 ; h<limit ;h=h+increment)</pre>

Compute  $\Phi$  and  $\Gamma$  for h

Compute discrete poles for h

Compute gains for h

Compute IAE

{

}

For non adapted controllers						
Precompute nominal gains for h <sub>i</sub>						
For(h=0 ; h <limit ;h="h+increment)&lt;/td"><td></td></limit>						
{						
Compute Ad,Bd for h						
Compute discrete poles for h						
Compute IAE						
}	133					

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## Control of computing systems

### Key aspects in "control of RT control systems"

#### IAE degradation diagram for adapted controllers, general aspect:



## Control of computing systems Key aspects in "control of RT control systems"

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IAE degradation diagram for adapted controllers, general aspect:





## Control of computing systems

## Key aspects in "control of RT control systems"

 Is the degradation caused by platform constraints always the same regardless of the control design methodology? NO





Direct discrete design (ddd)

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### Key aspects in "control of RT control systems"

#### IAE degradation diagrams (approximation) for non-adapted controllers





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## Control of computing systems

### Key aspects in "control of RT control systems"

#### Guidelines for co-design

- They give an idea of how near to a correct design we are. If the curve (for non adapted controllers) goes up quickly, then the system is near to the limits (i.e., it degrades quickly) and, probably, jitters effects will be more noticeable. If curve is flat (almost flat) then we have some guaranties that the response will be closer to the one we expect. Useful for designing control of QoC
- They are useful for designing a set of controllers for overload conditions. A flat curve (for adapted controllers) indicates that dynamics will be invariant under processor overloads. We can allow the kernel to change sampling periods at execution time and then select the correct controller knowing that the response will not be affected

### Key aspects in "control of RT control systems"

#### Guidelines for co-design

... useful for slack reclaiming approaches for improving control in RTCS

It is well accepted than running a controller faster means to obtain a better response

Not always !!!





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## Control of computing systems

### Key aspects in "control of RT control systems"

#### **Guidelines for co-design**

... useful in overload conditions for controlling QoC





It makes sense to switch controllers



It does not

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### Slack reclaiming: optimal state feedback





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## Control of computing systems

### Slack reclaiming: optimal state feedback



Example on an inverted pendulum

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### **Slack reclaiming: optimal state feedback**



- Control System:
  - Flexible controller: capable of running with different frequencies, i.e. h in [h<sub>min</sub>...h<sub>max</sub>]
  - Provide useful feedback information to OS
- Operating System:
  - Real-Time: guarantee time constraints
  - Dynamic and flexible resource allocation (e.g., RBED, Elastic)

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## Control of computing systems

### Slack reclaiming: optimal state feedback

#### Static and dynamic feedback

• Static: performance (P) vs period (h):

$$\Rightarrow P(h) = \frac{\beta}{h} \quad \oplus \quad r = \frac{c}{h}$$

$$P(r) = \frac{\beta}{c} \quad r = \alpha \cdot r$$
Dynamic: States of controlled system
$$x_i(t)$$

$$E(t) = |x(t)| = \sqrt{x_1^2(t) + \dots + x_n^2(t)}$$

$$\alpha \cdot E \quad \text{State Feedback}$$

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### Slack reclaiming: optimal state feedback

#### **Resource allocation problem**





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# Control of computing systems

### Slack reclaiming: optimal state feedback

 Problem: Find [r<sub>1</sub>, .., r<sub>n</sub>] such as the sum of all control performance benefits is maximized, subject to the schedulability constraints U<sub>d</sub>

Maximize 
$$\sum_{i=1}^{n} P_i(r_i) E_i$$
  
subject to  $\sum_{i=1}^{n} r_i \le U_d$ 

• Solution:  $r_i = 0 (1 \le i \le n, i \ne j)$ , and  $r_j = U_d$ 

(assign all desired CPU to one task)

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Slack reclaiming: optimal state feedback



 $\mathcal{F}_i = \frac{\alpha_i}{\sum \alpha_j} \cdot U_d$ 

#### Slack reclaiming: optimal state feedback

- System Configurations
  - RBED: Resource-rate Based Earliest Deadline scheduling
  - Linux 2.4.20
- Workloads

d Systems Desian

Controller

- 3 inverted pendulums, each one with the same controller
  - *worst execution time* = 13.5ms, *period* = [30ms ... 50ms]
  - Discrete: {30ms, 40ms, 50ms}
- Random perturbations with different intervals
- Performance metrics
  - Control: cumulative error (IAE) =  $\int_{0}^{t} \sum_{i=1}^{4} |x_i(t)| dt$

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Control of computing systems

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- CPU usage and overhead

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 $h_i := h_i^{next}$  $x_i := \mathbf{read\_input}()$  $u_i :=$ calculate\_output $(h_i)$ ; send\_output $(u_i)$  $x_i^{next} := update\_state(x_i, h_i); e_i := |x_i^{next}|$  $r_i := \mathbf{rate\_adjust}(i, e_i)$  $h_i^{next} := \frac{c_i}{r_i}$  $\rightarrow$  rate\_adjust $(i, e_i)$ } if  $(e_i! = e_i^{old})$  $b_i := w_i e_i p_i$  $r_i^{next} :=$ **resource\_allocation** $(policy, b_i)$  $e_i^{old} := e_i$ return  $r_i^{next}$ } }

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Mean interval between perturbations: 4s



more frequent perturbations, optimal comparable to static less frequent, better optimal compared to static

Slack reclaiming: optimal state feedback



Context switch dominates Global and dynamic rate change: **negligible** 



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## Control of computing systems

Slack reclaiming: optimal state feedback

•Feedback policies improve control performance + save resources.

•Optimal outperforms others and improves by 25% in the best scenario.

•Overhead of optimal policy is negligible

Can it be done distributed?



### Slack reclaiming: optimal state feedback

Can it be done distributed? Yes

Problem: it requires having centralized the errors of all plants

Solution: using CAN network and its bitwise arbitration mechanism

Idea: each message identifier is inversely proportional to each plant error



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### Control of computing systems

Slack reclaiming: optimal state feedback







#### **Overload conditions**

Control in overload conditions (cpu, bandwidth): which is the minimum number of controllers required to keep a desired QoC?



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### Control of computing systems

#### **Overload conditions**

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#### **Overload conditions**

Minimize the number of controllers to be designed off line to keep the QoC within a given bound.

#### The user specifies:

QoC<br/>minminimum QoC levelε<br/>maxmaximum error (in %) w.r.t. the ideal envelop curve

#### Feasiblity analysis imposes:

T<sub>min</sub> minimum period for a controller

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#### **Overload conditions**

The error  $\epsilon_{\text{max}}$  allows to balance control performance with memory requirements:

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### Control of computing systems

#### **Overload conditions**

We tested our approach on an inverted pendulum. Three strategies have been compared.

Period range (ms) = [250, 540] System tick = 10 ms

**Optimal task** ( $\varepsilon_{max} = 0$ ). It requires 30 controllers.

Adaptive task ( $\varepsilon_{max} = 0.3$ ). It requires 4 controllers.

**Static task**. Single controller running at T = 540 ms.



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## Control of computing systems

#### **Overload conditions**

- method to cope with overload conditions in real-time control systems.
- The method allows using continuous rate adaptation mechanisms (e.g. elastic scheduling) for efficient resource exploitation.
- It allows minimizing the number of controllers to be designed off line (and memory requirements), while keeping a desired QoC performance.



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# Stability issues





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### **Conclusions**



### The end

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